

ENSACO 250 POWDER

a product of M.M.M. Carbon

Carbon black

Applications

Plastics -Silicon Rubber **Paints**

General characteristics

Formula: Carbon

Appearance: fine black powder

CAS nº: 1333-86-47

Standard packaging

7.5 kg bags 44 bags on one patiet

Typical data

· L		·
Average Particle Size determined by TEM	nm	40 <
Nitrogen Surface Area ASIM D-3037	m²/g	62.
DBP Absorption (*) ASIM D-2414	ml/100g	290
24M4 DBP Absorption (*) ASIM 0-3493	wl/1000	110
Density (in the bag)	Kg/m³	200
Ash Content ASIM D-1506	. %	0.01
Heating loss ASIM D-1509	%	0.10
Volatiles Content (105-C to 900-C)	%	0.15
Sieve Residue 325 mesh sieve and on 500 g DIN 53 580	ppm	2 · .
Sulfur content	%	0.01

(*) DBP Absorption determined by an Absorptometer equipped with a very soft, special spring and a capton black weight of 10g.



CARBON

MMM sia.

Av. Louise 534, 9te 1 - 1050 Brussels - Belgium Tel : (32-2) 627, 55"11 - Feet: (32-2) 627 53 93 - Tx : 21489 b

Appeldonistroot, 173, 2830 Wilebroek - Belglum eL: (32-3).886 7].81, Forc (32-3).886.42.73

US 6,627,693 B1

5

ν.

KILYK BOWERSOX PLLC

 Property	ASTM Procedure	
I ₂ No.	D-1510	
ČTAB	D-3765	
Tint	D-3265	
DBP	D-2414	
N ₂ SA	D-3037	

Table 1 sets forth the analytical properties of the carbon blacks of compounds 1-9. Compounds 2-9 contain furnace carbon blacks of the present invention. Compound 1 contains a conventional furnace carbon black control.

TABLE 1									
	1 N650	2 A	3 B	4 C	5 D	6 B	7 F	8 G	9 II
PNO	36	82	121	258	258	258	356	125	150
DBP	122	102	114	117	105	64	1.33	60	143
Tint	56	103	115	148	153	151	143	138	146
CTAB	38	82	111	167	211	240	251	125	150
N ₂ SA	38	83	119	200	220	230	367	125	150

1 = STERLING VH; 2 = VULCAN 3; 3 = VULCAN 6; 4 = BP700; 5 = BP800; 6 = BP900; 7 = CRX1449; 8 = REGAL 660; and 9 = CRX1444, all tradenames of Cabot Corporation.

The effectiveness and advantages of the present invention will be further illustrated by the rubber compositions set of forth in compounds 1-9. Table 2 sets forth the formulations of compounds 1-9. In preparing the rubber compositions, the method of mixing the components comprising the rubber composition is not critical. Any conventional method of mixing may be employed. In the present case, the mixing was performed in a Banbury mixer (1575 cc volume) utilizing the following procedure:

	STAGE 1: "BR" Banbury, 77RPM, 32° C. Water, 40PSI Ram			
0,	Load NR, BR			
30"	Load Black, Zinc Oxide, Steeric Acid, TMQ, 6PPD, Wax			
280° F.	Sweep, Add oil, increase RPM to 115			
300° F.	Dump. Sheet off on mill			

STAGE 2

On 49° C. Mill:

Add MB to mill and bend; Add TBBS and sulfur; $\delta{\times}6$ Milling

TABLE 2

Ingredient	PHR
Natural Rubber	40
BR	60
Carbon Black	*as indicated
Naphthenic Oil	*as indicated
Zinc Oxide	5
Stearic Acid	2
TMQ	1.5
6 PPD	1.5

TABLE 2-continued

 Ingredient	PHR	
Wax	1.5	
TBBS	1.5	
Sulfor	1.25	

The following test procedures were used to evaluate the physical properties of the rubber compositions of compounds 1-9:

15	Modulus, tensile, and clongation at break	D-412
	Flex Patigue-Cut Growth	MERL Mk IV, Sinusoidal mode, tested at 43° C.
	Abrasion Resistance Rebound	Akron Angle Abrader, 20° angle D-1054
20	Gloss Jetness	BYK-Gardner Micro TKI Gloss Meter Uniter Labscan 6000, 10°, D65 CIELAB Color Space

Most importantly, gloss was measured on tensile slabs not subjected to water using a BYK-Gardner Micro TKI Gloss meter under light reflecting at a 60° angle. Jetness was measured by the Hunter Labscan 6000, 10 degree, D65 CIELAB Color Space, measuring each compound versus a control sample containing N650 at 55 phr. Each compound was scanned for jetness (L*) five times, and the average reported.

Flex Fatigue-Cut growth was tested using a MERLMk IV Crack Growth Fatigue Machine under simusoidal mode at 43° C. +-3° C. with various strains to give varying tearing energies. The test piece is a vulcanized strip of rubber containing a man made incision.

Table 3 sets forth the physical properties of the rubber compositions of selected compounds. The results show that the rubber compositions containing carbon black D, under the present invention, exhibit higher gloss and lower jetness as compared with rubber compositions of compound 1 utilizing the control furnace black ASTM N650. The Table 3 data further shows that the rubber compositions of the present invention may contain lower loadings of carbon black when compared to the compositions utilizing the control ASTM N650 carbon black. The results also indicate that rubber compositions prepared with the furnace carbon blacks of the present invention exhibit critical physical 50 properties such as flex fatigue (crack growth) comparable with those possessed by the compositions containing the control carbon black, N650. The results further indicate that the compositions containing the carbon blacks of the present invention show comparable results in critical properties such as tensile strength and advantages in abrasion resistance. These failure properties can be of particular advantage in rubber articles which come into contact with abrasive or sharp surfaces, such as tire sidewalls. The Figure shows tearing energy versus cut growth, demonstrating the advan-tage in flex fatigue at all tearing energies for the rubber compositions of the present invention when compared to the control, N650. Last, it is noted that the rubber compositions containing the carbon blacks of the present invention exhibit higher hysteresis (lower rebound), but lower loadings of the 65 carbon blacks of the present invention minimize this apparent deficiency while maintaining a very high level of reinforcement.